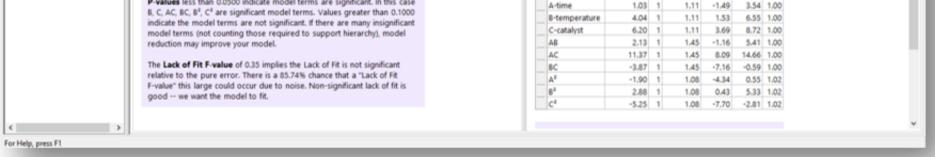
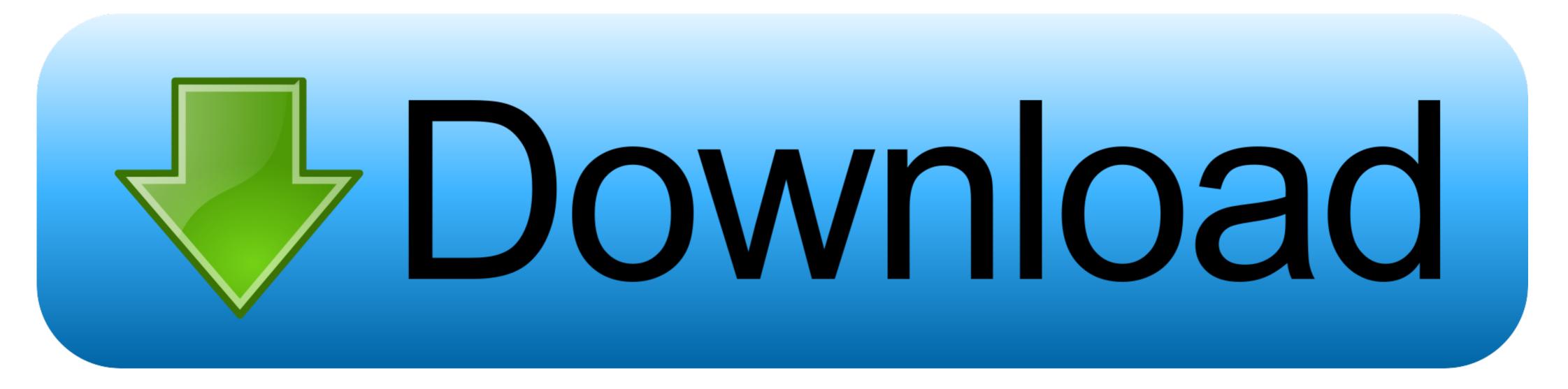


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Sumarysis       Static       Static <th>Factor coding is Coded.         Static reprinted         Analysis         right conversion (Analyzed)         minetical         raphical         Analysis         right conversion (Analyzed)         minetical         Stat. Dev. 4.11         Residual         Source       Stat. Dev. 4.11         Residual       1         B*temperature       222.96         1       222.96         2.22.96       1</th> <th></th> <th colspan="7">,</th> <th colspan="6">Fit Statistics</th>	Factor coding is Coded.         Static reprinted         Analysis         right conversion (Analyzed)         minetical         raphical         Analysis         right conversion (Analyzed)         minetical         Stat. Dev. 4.11         Residual         Source       Stat. Dev. 4.11         Residual       1         B*temperature       222.96         1       222.96         2.22.96       1		,							Fit Statistics						
Factor coding is Coded.         Sum of squares is Type III - Partial         Source       Sum of squares is Type III - Partial         Source       Sum of squares is Type III - Partial         Source       Sum of squares is Type III - Partial         Source       Sum of squares is Type III - Partial         Source       Sum of squares is Type III - Partial         Source       Sum of squares is Type III - Partial         Source       Sum of squares is Type III - Partial         Source       Sum of squares is Type III - Partial         Source       Sum of squares is Type III - Partial         Source       Sum of display       Provalue p-value p-value         Block       64.53       1       64.53       0         Coefficients Table       Block       64.53       1       64.53       0         Coefficients Table       Adjusted R <sup>1</sup> 1.4.44       1.4.44       0.86       0.3790         Adgusted R <sup>2</sup> of 0.8881; i.e. the difference is less than 0.2.       Adeq Precision measures the signal to noise ratio. A ratio greater than 4 is desirable. Your ratio of 16.294 indicates an adequate signal. This model can be used to navigate the design space.	Source       Source       Sum of squares is Type III - Partial         Source       Source       Sum of squares is Type III - Partial         Imposition       Source       Source       Sum of difference       P-value         Analysis       Biock       64.53       64.53       Field       Adjusted R <sup>2</sup> 0.0881         Model       2561.82       9       284.65       16.87       0.0001       significant         A-time       14.44       1       14.44       0.86       0.3790       The Predicted R <sup>2</sup> 0.7091 is in reasonable agreement with the         Adjusted R <sup>3</sup> 0.0135.12       1       0.0054       C-catalyst       525.44       1       525.42       1.0054       C-catalyst       525.44       1       525.44       1.15       0.0003       adequares signal. This model can be used to navigate the design space.         B       1035.12       1       1035.12       0.0257       adaguate signal. This model can be used to navigate the design space.       B <sup>2</sup> Coefficients       Education       Actual Equation         B <sup>3</sup> 119.19       1       119.19       7.06       0.0261       C <sup>2</sup> 397.61       397.61       23.97       0.009         Lack of FR       46.60       5       9.32		interporter 1. conv	Nesponse 1. Somersion							End Dav	411	e1	0.0440		
Sum of squares is type iii - partial         Sum of squares is type iii - partial         Numerical Graphical Post Analysis       Source       Sum of squares if type iii - partial         © Point Prediction       Source       Sum of squares if type iii - partial         © Confirmation       Geodificients Table       Model       2561.82       9       284.65       16.87       0.0001       significant         Coefficients Table       Model       255.64       1       252.64       1       252.64       Attion       Attion         A -time       1.4.44       1       1.4.44       0.86       0.3790       Adjusted R <sup>4</sup> of 0.8881; i.e. the difference is less than 0.2.         Adeq Precision measures the signal to noise ratio.       A ratio greater than 4 is desirable. Your ratio of 16.294 indicates an adequate signal. This model can be used to navigate the design space.       Adeq precision measures the signal to noise ratio. A ratio greater than 4 is desirable. Your ratio of 16.294 indicates an adequate signal. This model can be used to navigate the design space.	Sum of squares is type in - partain         Sum of squares is type in - partain         Sum of squares is type in - partain         Source       Sum of d         Block       64.53         Block       64.53         Bodel       2561.82         B-temperature       222.96         14.44       14.44         0.613       22.96         14.22.96       1.22.96         15.12       1.0051         C-catalyst       525.64         1       119.19         AC       1035.12         B <sup>1</sup> 119.19         B <sup>2</sup> 119.19         B <sup>3</sup> 119.19         C <sup>4</sup> 397.61         B <sup>3</sup> 119.19         C <sup>4</sup> 397.61         B <sup>3</sup> 119.19         C <sup>4</sup> 397.61 </td <td></td> <td colspan="7" rowspan="2"></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>															
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Graphical Post Analysis       Source       Source       Source       Source       Source       Final value       p-value         © Point Prediction       © Confirmation       Ellock       64.53       1       6	Source         Source         Source         Source         F-value         p-value           Analysis         Source         Source         Source         F-value         p-value         Image: Source         Source         Source         F-value         p-value         Image: Source         Source         Source         Source         Source         F-value         p-value         Image: Source         Sourc											512.5				
Block         64.53         1 </td <td>Block         64.53         1         64.53         C         C           onfirmation oefficients Table         Model         2561.82         9         284.65         16.87         0.0001         significant           A-time         14.44         1         14.44         0.86         0.3790         C           B-temperature         222.96         1         222.96         13.21         0.0003         C           AB         36.13         1         36.13         2.14         0.1774         C           AC         1035.12         1         1035.12         61.0027         C         Color         <t< td=""><td>Source</td><td></td><td>df</td><td></td><td>F-value</td><td>p-value</td><td></td><td></td><td></td><td></td><td>, and , record</td><td>104.944</td><td></td></t<></td>	Block         64.53         1         64.53         C         C           onfirmation oefficients Table         Model         2561.82         9         284.65         16.87         0.0001         significant           A-time         14.44         1         14.44         0.86         0.3790         C           B-temperature         222.96         1         222.96         13.21         0.0003         C           AB         36.13         1         36.13         2.14         0.1774         C           AC         1035.12         1         1035.12         61.0027         C         Color         Color <t< td=""><td>Source</td><td></td><td>df</td><td></td><td>F-value</td><td>p-value</td><td></td><td></td><td></td><td></td><td>, and , record</td><td>104.944</td><td></td></t<>		Source		df		F-value	p-value					, and , record	104.944		
Model         2561.82         9         284.65         16.87         0.0001 significant         Adjusted R <sup>2</sup> of 0.8881; i.e. the difference is less than 0.2.           Coefficients Table         A-time         14.44         1         14.44         0.86         0.3790         Adjusted R <sup>2</sup> of 0.8881; i.e. the difference is less than 0.2.           B-temperature         222.96         1         222.96         13.21         0.0054         Adjusted R <sup>2</sup> of 0.8881; i.e. the difference is less than 0.2.           C-catalyst         525.64         1         525.64         1         525.64         31.15         0.0003           AB         36.13         1         36.13         2.14         0.1774         adequate signal. This model can be used to navigate the design space.         space.	Model         2561.82         9         284.65         16.87         0.0001         significant           oefficients Table         A-time         14.44         1         14.44         0.86         0.3790           B-temperature         222.96         1         222.96         13.21         0.0054           C-catalyst         525.64         1         525.64         31.15         0.0003           AB         36.13         1         36.13         2.14         0.1774           AC         1035.12         1         102.12         7.12         0.0257           A <sup>4</sup> 51.76         1         51.76         0.07         0.1138           B <sup>4</sup> 119.19         1         10.91         0.0257           A <sup>4</sup> 51.76         3.07         0.1138           B <sup>4</sup> 19.19         7.06         0.0261           C <sup>4</sup> 397.61         1         397.61         23.57         0.0009           Residual         151.85         9         16.87         0.0261         C           C <sup>4</sup> 397.61         1         397.61         23.57         0.0009           Residual         151.85         9 </td <td></td> <td>Block</td> <td>64.53</td> <td>1</td> <td>64.53</td> <td></td> <td></td> <td></td> <td></td> <td colspan="6">The Predicted R<sup>a</sup> of 0.7891 is in reasonable agreement with the</td>		Block	64.53	1	64.53					The Predicted R <sup>a</sup> of 0.7891 is in reasonable agreement with the					
B-temperature         222.96         1         222.96         13.21         0.0054           C-catalyst         525.64         1         525.64         31.15         0.0003           AB         36.13         1         36.13         2.14         0.1774           AC         1035.12         1         1035.12         61.35         < 0.0001	B-temperature       222.96       1       222.96       13.21       0.0054         C-catalyst       525.64       1       525.64       1       525.64       31.15       0.0003         AB       36.13       1       36.13       2.14       0.1774         AC       1035.12       1       1035.12       61.35       < 0.0001         BC       120.12       1       120.12       7.12       0.0257         A <sup>2</sup> 51.76       1       51.76       3.07       0.1138         B <sup>4</sup> 119.19       1       19.19       7.00       0.0261         C <sup>4</sup> 351.76       1       32.37       0.0009       B       Coefficients       Coded Equation       Actual Equation         Residual       151.85       9       16.87       0.35       0.8009       0.8574       0.		Model	2561.82	9	284.65	16.87	0.0001	significant		Adjusted R <sup>2</sup> of 0.8881; i.e. the difference is less than 0.2.					
Stemperature         222.90         1         222.90         15.21         000034           C-catalyst         525.64         1         525.64         31.15         0.0003           AB         36.13         1         36.13         2.14         0.1774           AC         1035.12         1         1035.12         61.35         < 0.0001	B*temperature       222:30       1       222:30       1       222:30       1       222:30       1       222:30       1       222:30       1       222:30       1       222:30       1       222:30       1       222:30       1       222:30       1       22:30       1       30:31       2       1       0:0034       greater than 4 is desirable. Your ratio of 16:294 indicates an adequate signal. This model can be used to navigate the design space.         AB       36:13       1       103:512       61:135       < 0:0021	Coefficients Table	A-time	14.44	1	14.44	0.86	0.3790								
C-catalyst         525.64         1         525.64         31.15         0.0003           AB         36.13         1         36.13         2.14         0.1774           AC         1035.12         1         1035.12         61.35         < 0.0001	C-catalyst       525.64       1       525.64       31.15       0.0003         AB       36.13       1       36.13       2.14       0.1774         AC       1035.12       1       1035.12       61.35       < 0.0001		8-temperature	222.96	1	222.96	13.21	0.0054								
AB 36.13 1 36.13 2.14 0.1774 AC 1035.12 1 1035.12 61.35 < 0.0001	AB       36.13       1       36.13       2.14       0.1774         AC       1035.12       1       1035.12       61.33       < 0.0001		C-catalyst	525.64	1	525.64	31.15	0.0003								
AC 1035.12 1 1035.12 61.35 < 0.0001	AC       1035.12       1       1035.12       61.35       < 0.0001		A8	36.13	1	36.13	2.14	0.1774					in the used to harry	are the des		
BC 120.12 1 120.12 7.12 0.0257	A <sup>2</sup> 51.76       1       51.76       3.07       0.1138         B <sup>3</sup> 119.19       1       119.19       7.06       0.0261         C <sup>2</sup> 397.61       1       397.61       23.57       0.0009         Residual       151.85       9       16.87       Coded Equation       Actual Equation         Lack of Fit       46.60       5       9.32       0.35       0.8574 not significant       Coefficients in Terms of Coded Factors         Pure Error       105.25       4       26.31		AC	1035.12	1	1035.12	61.35	< 0.0001								
	B <sup>3</sup> 119.19         1         119.19         7.06         0.0261           C <sup>4</sup> 397.61         1         397.61         23.57         0.0009           Residual         151.85         9         16.87         Coefficients         Coded Equation         Actual Equation           Lack of Fit         46.60         5         9.32         0.35         0.8574         not significant           Pure Error         105.25         4         26.31         Coefficients         Coefficients in Terms of Coded Factors		8C	120.12	1	120.12	7.12	0.0257								
A <sup>2</sup> 51.76 1 51.76 3.07 0.1138	C <sup>2</sup> 397.61         1         397.61         23.57         0.0009           Residual         151.85         9         16.87         Coefficients         Coded Equation         Actual Equation           Lack of Fit         46.60         5         9.32         0.35         0.8574 not significant         Coefficients in Terms of Coded Factors           Pure Error         105.25         4         26.31         Coefficients         Coefficients         Coefficients		A <sup>2</sup>	51.76	1	51.76	3.07	0.1138								
	Residual         151.85         9         16.87           Lack of Fit         46.60         5         9.32         0.35         0.8574 not significant           Pure Error         105.25         4         26.31         Coefficients in Terms of Coded Factors			119.19	1	119.19	7.06	0.0261								
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	Pure Error 105.25 4 26.31		Residual	151.85	9	16.87										
Lack of Fit 46.60 5 9.32 0.35 0.8574 not significant Coefficients in Terms of Coded Factors			Lack of Fit	46.60	5	9.32	0.35	0.8574	not significant		Coefficients in Terms of Coded Factors					
Pure Error 105.25 4 26.31			Pure Error	105.25	-4	26.31										
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